

FABRICATION AND EXPERIMENTAL INVESTIGATION OF PCM CAPSULES INTEGRATED IN SOLAR CABINET DRYER

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ABSTRACT

Solar dryer with heat storage material can reduce the drying time and assist to maintain the better quality of medicinal plant. Solar cabinet dryer integrated with thermal storage system by using phase change material (PCM) for drying of tubular roots was designed, fabricated and tested at Department of Unconventional Energy Sources and Electrical Engineering, Dr. Panjabrao Deshmukh Krishi Vidyapeeth, Akola. The system consists of flat plate solar collector, transparent cover, absorber plate, insulation, drying chamber, chimney and heat exchanger with PCM capsules to store heat during sunshine hours and release it during non-sunshine hours. In present heat storage units paraffin wax used as a PCM encapsulated of thirty four aluminum cylindrical capsules were equally spaced at a distance of 2.5 mm. The inlet and outlet air temperature and thermal storage efficiency of the solar dryer system has been studied. Experimental results indicated that the average drying efficiency of solar dryer was 15.6 percent and 18.8 percent and the average thermal energy storage efficiency was 57.01 per cent and 57.20 per cent in summer and winter respectively. It reveals that temperature of drying chamber increased by 12.64°C and 15.03°C over the average ambient temperature in summer and winter respectively. From the study it is concluded that the heat storage material stored maximum amount of heat during sunshine hours inside the air heater through heat exchanger and drying takes place more effectively during non sunshine hours for extended time of 4 to 5 hours.

Keyword: Solar cabinet dryer, Thermal energy storage, PCM capsule, Tubular roots

INTRODUCTION

Solar energy is the most attractive alternative energy sources for the future. Utilization of solar energy for drying of various agricultural commodities/produce is in practice since time immemorial for preservation of food and agricultural crops (Al-Busoul 2017). Solar drying

is a simple process of moisture removal from a product in order to reach the desired moisture content and is an energy intensive operation (Gutti et al. 2018). The prime objective of drying apart from extended storage life can also be to enhance quality, ease of handling, further processing and sanitation and is probably the oldest method of food preservation practiced by humankind (Deshpande 2018, Phadke et al. 2015, Tiwari, 2016). Drying involves the application of heat to vaporize moisture and some means of removing water vapor after its separation from the food products. It is thus a combined and simultaneous heat and mass transfer operation for which energy must be supplied (Zhang 2011, Ekechukwu 1999]. The removal of moisture prevents the growth and reproduction of microorganisms like bacteria, yeasts and molds causing decay and minimizes many of the moisture-mediated deteriorative reactions (Van Arsdell, 1965). Drying in earlier times was done primarily in the sun, now many types of sophisticated equipments and methods are used to dehydrate foods (Shafiur Rahman).

Energy storage is not only plays an important role in conservation of energy but also improves the performance and reliability of wide range of energy systems, and become more important where the energy source is intermittent such as solar (Alkilani et al. 2009). Energy storage process can reduce the rate mismatch between energy supply and energy demand (Dincer & Rosen 2007, Ermis & Findik 2020, Kuravi 2013]. The thermal energy storage is used in places where there is a variation in solar energy or in areas where there is a high difference of temperature between day and night (Alkilani et al. 2011). There are many thermal energy storage (TES) materials available for solar thermal applications among which a few have been investigated by experimental testing previously. Among these materials, the most common materials are the rock beds, pebble beds, aluminum composites, water, and paraffin wax. Most of the materials have a good capacity to store the heat and release this heat at a desired temperature up to a long period during off-sunshine hours for a heating task (Saxena et al. 2012, Goyal et al. 1998 & Farid et al. 2004).

Amongst thermal heat storage techniques, latent heat thermal energy storage is particularly attractive due to its ability to provide high energy storage density and its characteristic to store heat at constant temperature corresponding to the phase transition temperature of the PCM (Lane 1983, Abhat 1983). Latent heat storage is one of the most efficient ways of storing thermal energy (Mondal 2008). Latent TES system store energy in PCMs, with the thermal energy stored when the material changes phase, usually from a solid to liquid. A phase-change material (PCM) is a substance with a high heat of fusion which on melting and solidifying at a certain temperature, is capable of storing and releasing large amounts of energy. Heat is absorbed or released when the material changes from solid to liquid and vice versa (Arun Kumar & Shukla 2015). As the source temperature rises, the chemical bonds within the PCM break up as the material changes phase from solid to liquid (as is the case for solid-liquid PCMs, which are of particular interest here). The phase change is a heat-seeking (endothermic) process and therefore, the PCM absorbs heat. Upon storing heat in the storage material, the material begins to melt when the phase change temperature is reached. The temperature then stays constant until the melting process is finished (Sharma 2005, Regin 2008, Sharma 2009).

Selection of PCM is based on the application but the PCM to be use should possess thermophysical, kinetics and chemical properties and also availability and cost effectiveness of material(Himran et al. 2007, Lingayat 2013) The studies show that commercial grade paraffin wax and other pure paraffin's have stable properties after 1000-2000 cycles(Sharma 1999). Paraffin wax did not show regular degradation in its thermal properties after repeated melting/freezing cycles. Paraffin waxes are safe and non-reactive (Buddhi 1994). They are compatible with all metal containers and easily incorporated into heat storage systems (Lane 1980). Paraffin wax have been widely used for latent heat thermal energy storage system applications due to large latent heat and desirable thermal characteristics such as little or no super cooling, varied phase change temperature, low vapour pressure in the melt, good thermal and chemical stability and self nucleating behavior (Pablo et al. 2012). The number of carbon atoms present in the chains of paraffin wax which has melting temperatures between 30°C and 90°C ranges from 18 to 50 (C18-C50). The specific heat capacity of latent heat paraffin wax is about 2.1 kJ/kg °C. Their melting enthalpy of waxes lies between 180 and 230 J/g which is quite high for organic materials. Waxes are also readily available in market and inexpensive (Tan et al. 2009, Fan 2011). Utilization of PCM for thermal energy storage requires a proper heat exchanger system for charging and discharging the thermal energy (Stella 2012).

The aim of the present study is developed solar cabinet dryer which integrated with PCMs i.e. paraffin wax for drying of tubular roots and how much maximum amount of heat stored in heat storage material during sunshine hours inside the air heater and extended time takes for drying effectively during non sunshine hours. The testing of solar dryer was carried out at Department of Unconventional Energy Sources and Electrical Engineering, Dr. Panjabrao Deshmukh Krishi Vidyapeeth, Akola.

MATERIALS AND METHODS

Experimental Setup

The optimum design of solar air heaters based on PCM assumptions are made such as simple in design and operate, easy to maintain, performed in poor ambient conditions, inexpensive and have improved efficiency, significant improvement in product quality, no contamination by insects, micro organisms and mycotoxin, reduction in drying time and extension of drying period during non sunshine hours. Solar air heater with latent storage collector using spherical capsules as a packed bed absorber for drying of 10 kg/batch tubular roots was designed and fabricated. The experiment for no-load and full-load test was undertaken for drying of tubular crop. For evaluating the performance of solar dryer, full load test by using tubular roots was conducted during summer and winter respectively. The design takes into much consideration concern with simplicity in construction, integrated with PCM storage units, handling of PCM units, collector dimension are proposed accordance with Choudhury 1988, Fath 1994 and Enibe 2002.



Fig 1a: Experimental set up of solar cabinet dryer

Solar cabinet dryer

This system consists of drying chamber with heat exchanger and two chimneys. The insulation of glass wool with thickness of 2.5 cm are sandwiched between absorber plate and outer cover of solar cabinet dryer. The size of solar cabinet dryer are 1800 x 1000 x 150 mm having number of drying tray is five. The absorber plate with thickness of 2 mm painted black with selective coating having high absorptivity. Slit with flap are provided at one side of solar cabinet dryer and other side was connected with drying chamber. The physical dimension of this system is given in Table A.1. The drying chamber is directly connected to solar air heater. The drying chamber consists of five drying trays with two chimneys (Figure A.1).

Table A.1: Thermophysical dimension of tested solar cabinet dryer

PARAMETER	VALUE
Size of solar cabinet dryer, mm	1800 x 1000 x 150
Number of drying trays, no.	05
Exhaust fans	12V, DC, 0.35 A
Constructing material of air heater	GI sheet
Inclination of the solar air heater with respect to horizontal	27°
Global radiation at Akola, (I_{sc}), Wm^{-2}	700
Location	Dr.P.D.K.V.Akola
Longitude	77°10'E
Latitude	20°30'N

Fabrication of PCM capsules

Heat exchanger unit consists of stand for aluminum capsules filled with phase change medium i.e. paraffin wax. Thirty four (34) number of aluminum capsules spaced 2.5 mm apart were placed centrally in between absorber plate and glass cover. The aluminum capsules were coated with selective black paint and then placed in the collector, arranged in a single row across the flow of air. The thermo-physical properties of paraffin wax were tested at Anacon Labs Pvt. Ltd. Nagpur given in Table A.2 while the physical dimension of capsules is in Table A.3. The storage unit consists of 65 kg paraffin wax encapsulated in the set of 50 cm diameter aluminum tubes. It was used for providing stored heat during off-sunshine hours.

Table A.2: Thermophysical properties of Paraffin wax phase change material

PARAMETER	VALUE
Weight of Paraffin wax	65 kg
Specific heat	2.50 kJ/kgK
Thermal conductivity	0.28 W/mK
Latent heat of fusion	201 kJ/kg
Density	0.993 g/cm ³
Melting point	52°C

Table A.3: Thermophysical properties of heat storage system

PARAMETER	VALUE
No. of aluminum pipes of heat exchanger	34
Diameter of aluminum pipe, mm	50
Length of aluminum pipe, mm	980
Spacing between aluminum pipe, mm	2.5
Weight of aluminum pipe, kg	23
Size of aluminum absorber plate, mm	1800 x 1000 x 2

The capsule ends were sealed by nylon caps fixed by screws and araldite. The paraffin blocks were shredded into small pieces for easy melting then poured inside the tube via a big screwed hole made in order to reuse the capsule many times, such as if need to add some additives to enhance heat transfer or change the entire storage medium. The screw was closed when the tube was filled with paraffin wax in liquid phase, so as to reduce the PCM pressure during charging process (Figure A.2). All these precautions were taken to prevent any leakage or expansion problems.



FigA.2: Capsule filling process with paraffin wax

Theoretical background: Thermal Energy Storage Efficiency (η_t)

During discharge process when no radiation and the PCM was initially at liquid phase. According to law of conservation of energy, energy stored in to the thermal storage unit is equal to energy extracted from it. The thermal energy storage efficiency was calculated as follows (Alkila ni 2011)-

$$(T_{in} - T_{out})C_a \dot{m} = 2\pi R_o l h (T_m - T_{sfc}) + \varepsilon A \sigma (T_{sfc}^4 - T_{sur}^4) \text{ Eq. (1a)}$$

Where,

T_{in} = Air temperature before the cylinder ($^{\circ}\text{C}$)

T_{out} = Air temperature after the cylinder ($^{\circ}\text{C}$)

C_a = Specific heat for air ($\text{kJ kg}^{-1} \text{ } ^{\circ}\text{C}^{-1}$)

\dot{m} = Mass flow rate (kg s^{-1})

R_o = Outer radius (m)

l = Capsule length (m)

h = Heat transfer coefficient ($\text{kJ m}^{-2} \text{s}^{-1} \text{ } ^{\circ}\text{C}^{-1}$)

T_{sfc} = Capsule surface temperature ($^{\circ}\text{C}$)

ε = Emissivity (-)

A = Capsule area (m^2)

σ = Stephan-Boltzman constant ($\text{kW m}^{-2} \text{K}^{-4}$)

T_{sur} = Surrounding temperature (°C)

T_m = Melting temperature (°C)

The heat transfer coefficient of flow normal to bank of tubes in line approximated (McAdams, 1954):

$$h = \frac{K_a}{D_o} b_2 Re^n \quad \text{Eq. (2a)}$$

Where,

K_a = Thermal conductivity of air (kWm⁻¹°C⁻¹);

D_o = Outside diameter (m);

Re = Reynolds number (-);

b_2 and n = Constant equal to 0.3 and 0.6 respectively

The efficiency of thermal energy storage systems can be defined as the ratio of the energy extracted from the thermal storage unit to the energy stored into it. The following equation has been used to compute the efficiency of thermal energy storage:

$$\eta = \frac{[(T_{in} - T_{out}) C_a \dot{m}]}{\{[(T_{in} - T_{out}) C_a \dot{m}] + 2\pi R_o l h(T_m - T_{sfc}) + \epsilon A \sigma (T_{sfc}^4 - T_{sur}^4)\}} \quad \text{Eq. (4a)}$$

$(T_{in} - T_{out}) C_a \dot{m}$ = TE efficiency (%)

Q_o = Heat retrievable from TES (kW)

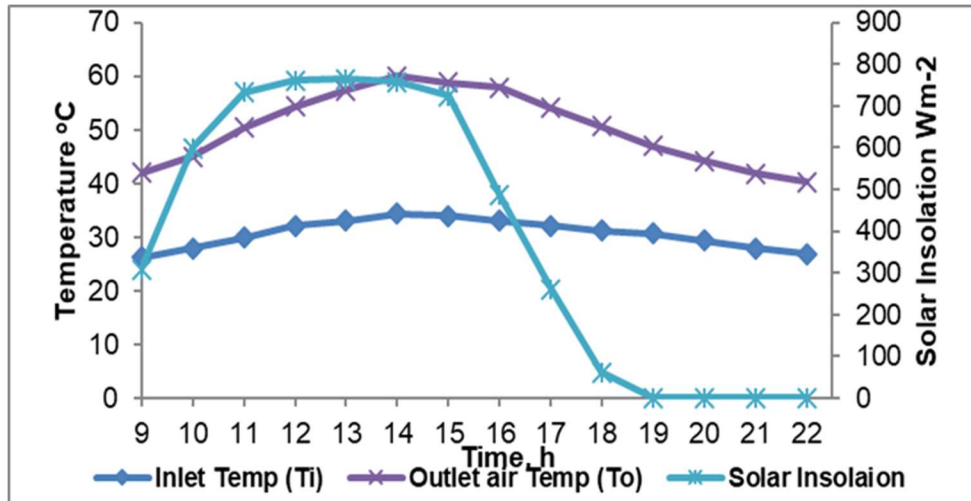
Q_L = Heat lost to the environment (kW)

$$\eta = \frac{[(T_{in} - T_{out}) C_a \dot{m}]}{\{[(T_{in} - T_{out}) C_a \dot{m}] + 2\pi R_o l h(T_m - T_{sfc}) + \epsilon A \sigma (T_{sfc}^4 - T_{sur}^4)\}} \quad \text{Eq. (4a)}$$

RESULTS AND DISCUSSION

The experiment were carried out in solar cabinet dryer during no load and full load test and evaluate the performance of solar dryer without product during summer and winter season. The variation in temperature corresponding ambient temperature, solar radiation were recorded. The temperature developed in air heater at its inlet, and outlet were recorded to evaluate the performance of air heater integrated with thermal storage material i.e. paraffin wax in heat exchanger during summer and winter season. It was seen paraffin wax is used as PCM material in solar air heater to conserve heat during day and can be used as a source of heat in night. The melting of wax occurred during the study because maximum overheat above melting temperature was approximately 18.5K.

No load test: The average inlet temperature in drying chamber was 47.58°C corresponding to ambient temperature 30.65°C and average solar isolation of 545.40 Wm⁻² during no load test in winter. Average inlet and outlet temperature developed in air heater was 30.63°C and 50.67°C during no load test in winter. It reveal that the average temperature difference of 19.94°C was found between inlet and outlet temperature in air heater and 16.94°C was found between inlet temperature and average temperature in drying chamber (Fig.A.3).



FigA.3: Average temperature developed in air heater during no load test in winter season

The average inlet temperature in drying chamber was 47.84°C corresponding to ambient temperature 34.72°C and average solar insolation of 602.62 Wm⁻² during no load test in summer. Average inlet and outlet temperature developed in air heater was 34.74°C and 51.31°C during no load test in summer. It seen that average temperature difference of 16.57°C was found between inlet and outlet temperature in air heater and temperature difference of 13.10°C was found between inlet temperature and average temperature in drying chamber during summer (Fig.A.4).

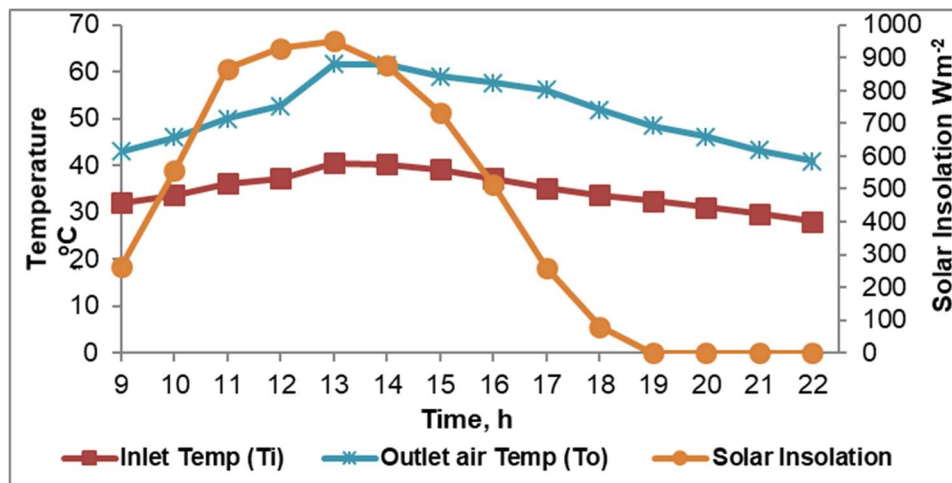
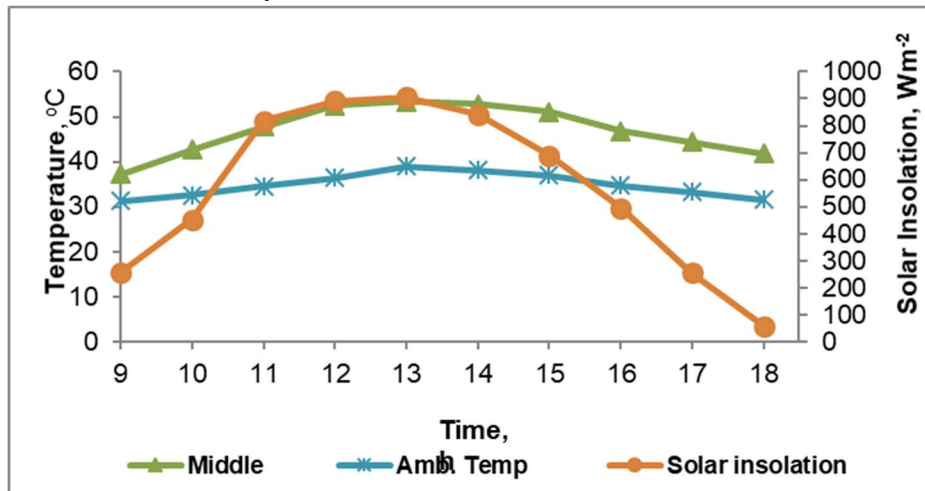


Fig.A.4: Average temperature developed in air heater during no load test in summer season

Full load test: Full load test of solar dryer was conducted by drying fresh tubular roots in summer and winter season.

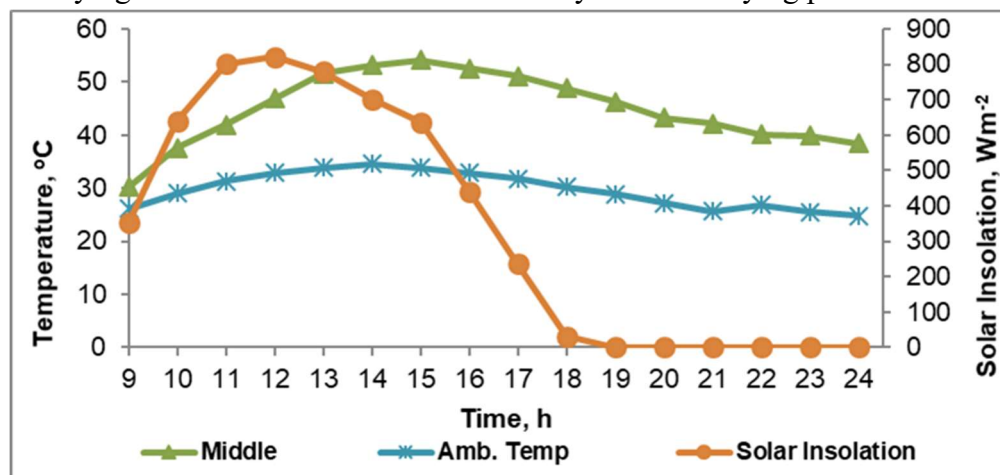
The average temperature inside the solar dryer and relative humidity was found 47.58°C and 24.40 per cent corresponding to average ambient temperature, ambient relative humidity and solar insolation were 34.84°C, 18 per cent and 566.61 Wm⁻² respectively during load test in summer (Fig A.5). It is observed that the temperature of drying chamber was increased by 12.64°C over the

average ambient temperature, whereas average relative humidity was reduced by 6.40 per cent than average ambient relative humidity.



FigA.5: Average variation of temperature during full load test of dryer in summer

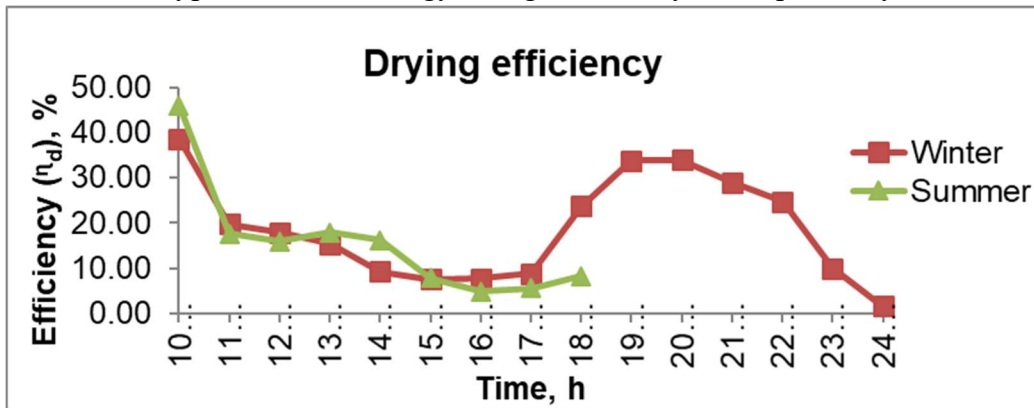
It is observed that the temperature of drying chamber and relative humidity was 44.74°C and 19.38 per cent (Fig A.6). It reveals that temperature of drying chamber increased by 15.03°C over the average ambient temperature, whereas average relative humidity was reduced by 12.06 per cent than average ambient relative humidity in winter. The average ambient temperatures, relative humidity inside the dryer and solar insolation were 29.71°C, 31.19 per cent and 544.00 Wm⁻² respectively in winter. It was observed that the increase in temperature inside the drying chamber correspondingly reduced the relative humidity to its lowest value attributed to the stored heat in the thermal heat storage system of air heater. It is revealed from the above results that the temperature required for drying was maintained inside the solar dryer for the drying process because of PCM.



FigA.6: Average variation of temperature during full load test of dryer in winter

The average drying efficiency of solar dryer was 15.6 percent and 18.8 percent in summer and winter respectively. Drying efficiency of solar dryer was highest at initial hours, i.e. 45.92 percent in summer and it was maximum, i.e. 38.68 percent during sunshine hours and 33.93 per cent

during non-sunshine hours in winter season. Thermal energy storage efficiency was 70.18 per cent and 69.00 per cent in summer and winter respectively at 9:00 h and it reduced to 46.58 per cent at 16:00 h in summer and 43.76 per cent at 14:00 h in winter, afterward thermal energy storage efficiency increased gradually to 72.29 per cent in summer and 72.76 per cent in winter at 22:00 h (Fig A.7). The average thermal energy storage efficiency was 57.01 percent and 57.20 per cent in summer and winter respectively (Fig A.8). The heat storage material stored maximum amount of heat during sunshine hours inside the air heater through heat exchanger and drying takes place more effectively during non sunshine hours for extended time of 4 to 5 hours. Similar type of thermal energy storage efficiency was reported by Krishnananth 2013.



FigA.7: Variation in hourly drying efficiency during summer and winter

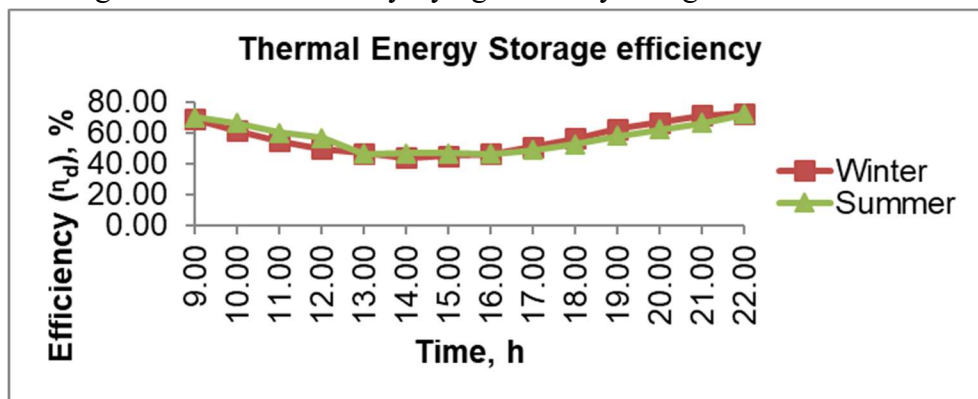


Fig A.8: Variation in hourly thermal energy storage efficiency during summer and winter

CONCLUSION:

The temperature required for drying was maintained inside the solar dryer for the drying process because of phase change material. The average drying efficiency of solar dryer was 15.6 percent and 18.8 percent and average thermal energy storage efficiency was 57.01 percent and 57.20 per cent in summer and winter respectively. Solar cabinet dryer integrated with PCM was found suitable for drying of medicinal plants effectively during summer and winter season. It reveals that temperature of drying chamber increased by 12.64°C and 15.03°C over the average ambient temperature in summer and winter respectively. Heat stored in phase change material can be utilized during non-sunshine hours to extend drying time upto 5 hours.

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